


## 24: Frequency Control

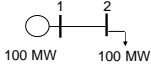
text: 11.6 – 11.12

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## Frequency Control

- We now look at how the frequency is controlled in the network
- Consider the lossless system operating at 60 Hz with:
  - $P_{G1} = 100$  MW
  - $P_{D2} = 100$  MW

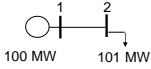


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## Frequency Control

- What happens if the load suddenly increases to 101 MW?
- If the power supplied to the generator's prime mover does not change, we have a mismatch of power between load and generation
- Where does this power come from?



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## Frequency Control

- Answer: the power is extracted from the rotating mass of the generator itself, causing it to slow in rotation (and eventually stop, if nothing is done)

$$T_m - T_e = J \frac{d\omega_{rm}}{dt}$$

- $T_m$ : mechanical torque from the prime mover
- $T_e$ : electromagnetic counter torque
- $J$ : mass polar moment of inertia of all rotating parts
- $\omega_{rm}$ : rotor shaft velocity in mechanical rad/s


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## Frequency Control

- Multiply by  $\omega_{rm}$  to get:
 
$$P_m - P_e = \omega_{rm} J \frac{d\omega_{rm}}{dt}$$
  - $P_m$ : mechanical power from the prime mover
  - $P_e$ : electromagnetic power torque
- So, if  $P_e > P_m$ , then the rotor slows down
  - frequency drops
- What happens to the frequency if the load decreases to 99 MW ?
  - frequency increases


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## Frequency Control

- Fluctuating frequency is not desirable
  - damages equipment
  - output power of pumps, fans, etc depend on system frequency
  - etc
- How do we prevent frequency deviations?
  - use deviation as a control signal to cause increases or decreases in prime mover power
  - essentially, we match generation with load
  - primary control: governor action to increase or decrease valve positions


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### Frequency Control

- Governor: see figure 11.1 in text for physical description of the governor
- The action of the governor can be simplified as
 
$$\Delta P_m = \Delta P_c - \frac{1}{R} \Delta \omega$$
  - $\Delta P_c$  : change in command input
  - R: regulation constant (Hz/MW) or (rad/sec/p.u. power) or just p.u.
  - $\Delta \omega$  : change in system frequency

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### Frequency Control

- Let  $\omega_0$  be the nominal frequency
- Let  $P_m = P_c$  (the generator is operating at its set-point)
- Now, the load increases causing decrease in frequency of  $\Delta \omega$
- The governor action increases the  $P_m$  to settle on a new operating point

$\Delta P_m = \Delta P_c - \frac{1}{R} \Delta \omega$

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### Frequency Control

- A common term is "droop": the variation of frequency with  $P_m$  and is related to R
- The less droop, the better the regulation
- If all the generators in the system are properly controlled, the power in the system returns to balance
- Additional control is required to increase the frequency back to nominal (and  $P_c$  changes)

$\Delta P_m = \Delta P_c - \frac{1}{R} \Delta \omega$


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### Example

- Let  $R = 0.05$  p.u. (also expressed as a percent)
- Suppose the frequency changes from 60 Hz to 59 Hz, what is the corresponding change in  $P_m$ ? (assume there is no change in control signal)

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### Example

- Let  $R = 0.05$  p.u. (also expressed as a percent)
- Suppose the frequency changes from 60 Hz to 59 Hz, what is the corresponding change in  $P_m$ ? (assume there is no change in control signal)


$$\Delta P_m = \Delta P_c - \frac{1}{R} \Delta \omega$$

$$\Delta P_m = 0 - \frac{1}{0.05} \left( \frac{-1}{60} \right)$$

$$\Delta P_m = 0.3333 \text{ p.u.}$$

← since R is in per unit, so should  $\Delta \omega$

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### Example

- If it was a 100 MW unit, the new power output would be 133 MW
- At what change in frequency would  $P_m$  change from 0 to 1 p.u. (no load to full load)?

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**Example**

- If it was a 100 MW unit, the new power output would be 133 MW
- At what change in frequency would  $P_m$  change from 0 to 1 p.u. (no load to full load)?

$$\Delta P_m = \Delta P_c - \frac{1}{R} \Delta \omega$$

$$1 = \frac{1}{0.05} (\Delta \omega)$$

$$\Delta \omega = 0.05 \text{ p.u.}$$

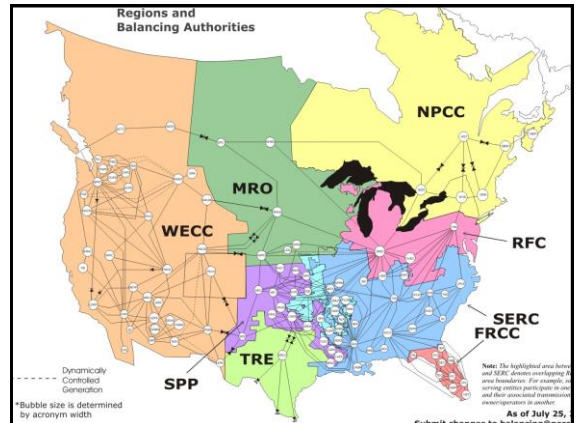
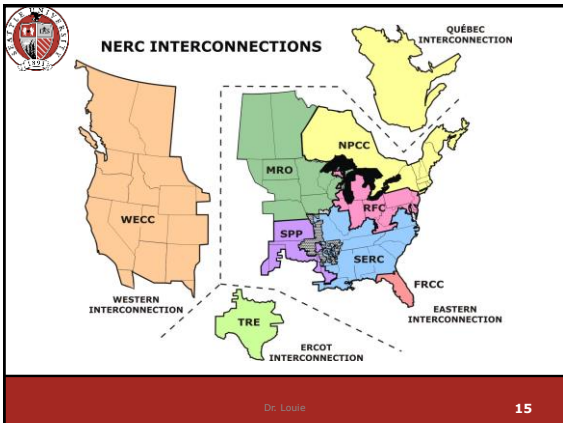
$$\omega = 57 \text{ Hz}$$

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**Frequency Control**

- How are the power command are determined by control area
- Control areas: groups of closely coupled generators
  - each control area is weakly coupled to other control areas
  - this greatly simplifies the model of the interconnected power system

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**Frequency Control**

- Consider two control areas
- Each control area can have many generators and loads, though they are not explicitly modeled. However, tie line connections are.
- Control areas can be used in the analysis of power pools

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**Frequency Control**

- A power pool is an interconnection of utilities
- Each operates independently within its jurisdiction, but there exist contractual agreements regarding inter-company exchanges of power and operating procedures to maintain system frequency

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### Frequency Control

- Basic principles of pool operation:
  - scheduled tie-line power interchanges are maintained
  - each area absorbs its own load changes
- These objectives do not apply to transients (faults, etc)

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### Frequency Control

- A slight digression...
- Assume that the tie-line carrying  $P_{12}$  from Area 1 to Area 2 is lost
- Change in frequency in Area 1 is
 
$$\Delta\omega_{1ss} = \frac{P_{12}}{\beta_1}$$
  - $\omega_{1ss}$ : steady state frequency
  - $\beta_1$ : frequency characteristic of Area 1

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### Frequency Control

- A similar expression for the change in steady state frequency in Area 2 can be found to be:
 
$$\Delta\omega_{2ss} = \frac{-P_{12}}{\beta_2}$$
- Now assume the line is added and the frequency in both areas is returned to normal
- If there is a sudden change in load in Area 2,  $P_{L2}$  and the tie-line power flow is **not** allowed to change then
 
$$\Delta\omega_2 = \frac{-\Delta P_{L2}}{\beta_2}$$

$$\Delta\omega_1 = 0$$

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### Frequency Control

- If we allow the power to change, then
 
$$\Delta\omega_2 = \Delta\omega_1 = \frac{-\Delta P_{L2}}{\beta_1 + \beta_2}$$
 and the tie-line power flow will also increase
- We can restore the system frequency to nominal by adjusting  $P_C^1$  and  $P_C^2$  (the command signals for each area)
- To determine the values, we are guided by the principles of pool operation

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### Frequency Control

- The adjustment of  $P_C^1$  and  $P_C^2$  is done automatically based on tie-line or secondary control
- The control is such that they drive the Area Control Error (ACE) to zero
 
$$ACE_1 = \Delta P_{12} + B_1 \Delta\omega$$

$$ACE_2 = \Delta P_{21} + B_2 \Delta\omega$$
  - $\Delta P_{12}$ ,  $\Delta P_{21}$  are the deviations from the scheduled interchange
  - $B_1$ ,  $B_2$  are the frequency bias settings and are positive
  - If load damping is ignored, then  $B_1 = 1/R_1$  and  $B_2 = 1/R_2$

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### Frequency Control

- Consider the following scenario with:
  - $P_{12}$  positive
  - Now assume the load  $P_{D2}$  in Area 2 increases

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### Frequency Control

- In the considered scenario with  $\Delta P_{D2}$  positive,  $P_{12}$  tends to increase above its scheduled value
  - $\Delta P_{12}$  is positive
  - $\Delta P_{21}$  is negative
- Since frequency is dropping,  $\Delta\omega$  is negative
  - $ACE_1 = \Delta P_{12} + B_1 \Delta\omega$
  - $ACE_2 = \Delta P_{21} + B_2 \Delta\omega$
- $ACE_2$  is negative
- $ACE_1$  should have a small magnitude


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### Frequency Control

- Since  $ACE_2$  is negative,  $P_C^2$  should increase
- We expect a smaller change for  $P_C^1$
- $ACE$  is used as metric for measuring area performance


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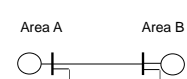
### Frequency Control


- North American Electric Reliability Corporation (NERC) criteria for control performance require that:
  - $ACE$  must equal zero at least one time in all 10-minute periods
  - average deviation of  $ACE$  from zero for all 10-minute periods must be within specified limits based on a percentage of system generation
- Performance criteria for disturbance conditions:
  - $ACE$  must be returned to zero within 10 minutes
  - corrective action must be forthcoming within one minute of a disturbance


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### Example

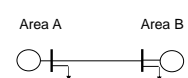
- Area A:  $P_D = 1000$  MW,  $P_G = 1000$  MW,  $R = 0.015$  rad per sec/MW
- Area B:  $P_D = 10,000$  MW,  $P_G = 10,000$  MW  $R = 0.0015$  rad per sec/MW
- $P_{AB} = 0$




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### Example


- A sudden load increase of 10 MW occurs in Area A
- Find the  $ACE$  in each area, the change in frequency and the appropriate control signals



Area A:  $P_D = 1000$  MW,  $P_G = 1000$  MW,  $R = 0.015$  rad per sec/MW

Area B:  $P_D = 10,000$  MW,  $P_G = 10,000$  MW  $R = 0.0015$  rad per sec/MW

$P_{AB} = 0$

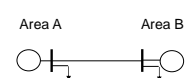

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### Example

- First find the frequency change:

$$\Delta\omega_A = \Delta\omega_B = \frac{-\Delta P_{DA}}{\beta_A + \beta_B}$$

$$\Delta\omega = \frac{-\Delta P_{DA}}{\beta_A + \beta_B} = \frac{-\Delta P_{DA}}{\frac{1}{R_A} + \frac{1}{R_B}} = \frac{-10}{\frac{1}{0.015} + \frac{1}{0.0015}} = -0.0136 \text{ rad/sec}$$




Area A:  $P_D = 1000$  MW,  $P_G = 1000$  MW,  $R = 0.015$  rad per sec/MW

Area B:  $P_D = 10,000$  MW,  $P_G = 10,000$  MW  $R = 0.0015$  rad per sec/MW

$P_{AB} = 0$

Load change: 10 MW increase in Area A


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**Example**

- The generators in each area respond:

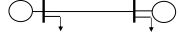
$$\Delta P_{GA} = -\frac{1}{R_A} \Delta \omega = -\frac{1}{0.015} (-0.0136) = 0.9091 \text{ MW}$$

Area A Area B

$$\Delta P_{GB} = -\frac{1}{R_B} \Delta \omega = -\frac{1}{0.0015} (-0.0136) = 9.091 \text{ MW}$$

- The tie-line change:

$$\Delta P_{AB} = -\Delta P_{AB} = \Delta P_{GA} - \Delta P_{LA} = 0.9091 - 10 = -9.091 \text{ MW}$$



Area A:  $P_D = 1000 \text{ MW}$ ,  $P_G = 1000 \text{ MW}$ ,  $R = 0.015 \text{ rad per sec/MW}$

Area B:  $P_D = 10,000 \text{ MW}$ ,  $P_G = 10,000 \text{ MW}$ ,  $R = 0.0015 \text{ rad per sec/MW}$

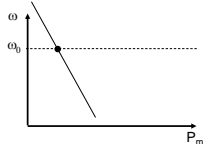
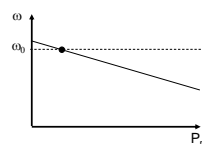
$P_{AB} = 0$

Frequency change:  $-0.0136 \text{ rad/sec}$

31

**Example**

- Which plot shows the response of Area A?

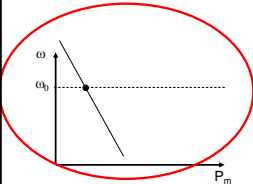
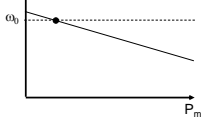



Area A:  $R = 0.015 \text{ rad per MW}$   
Area B:  $R = 0.0015 \text{ rad per MW}$

32

**Example**

- Which plot shows the response of Area A?

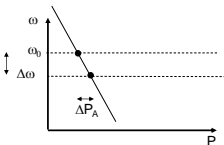
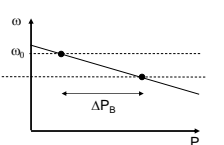



slope:  $= -R$       Area A:  $R = 0.015 \text{ rad per MW}$   
Area B:  $R = 0.0015 \text{ rad per MW}$

33

**Example**

- Area A has less load and generation so it is less capable of regulating large frequency changes


34

**Example**

- Now for the ACE

$$ACE_A = \Delta P_{AB} + \frac{1}{R_A} \Delta \omega = -9.091 + \left(\frac{1}{0.015}\right) (-0.0136) = -9.091 - 0.909 = -10 \text{ MW}$$

$$ACE_B = \Delta P_{BA} + \frac{1}{R_B} \Delta \omega = 9.091 + \left(\frac{1}{0.0015}\right) (-0.0136) = 9.091 - 9.091 = 0 \text{ MW}$$



Area A:  $P_D = 1000 \text{ MW}$ ,  $P_G = 1000 \text{ MW}$ ,  $R = 0.015 \text{ rad per sec/MW}$

Area B:  $P_D = 10,000 \text{ MW}$ ,  $P_G = 10,000 \text{ MW}$ ,  $R = 0.0015 \text{ rad per sec/MW}$

$P_{AB} = 0$

Frequency change:  $-0.0136 \text{ rad/sec}$

35

**Example**

- power command signals based on the ACEs will result in the generation in Area A increasing by 10 MW
- this matches the change in load and the tie-line flow returns to zero

36

**Example**

After supplementary control:

and the frequency is returned to nominal

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**Example**

- Area A:  $P_D = 1000$  MW,  $P_G = 1100$  MW,  $R = 0.015$  rad per sec/MW
- Area B:  $P_D = 9,900$  MW,  $P_G = 10,000$  MW  $R = 0.0015$  rad per sec/MW
- The load in Area A decreases by 20 MW
- Find the ACE in each area, the change in frequency and the appropriate control signals

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**Example**

- First find the frequency change:

$$\Delta\omega = \frac{-\Delta P_{DA}}{\beta_A + \beta_B} = \frac{-\Delta P_{DA}}{\frac{1}{R_A} + \frac{1}{R_B}} = \frac{20}{\frac{1}{0.015} + \frac{1}{0.0015}}$$

Area A      Area B

Area A:  $P_D = 1000$  MW,  $P_G = 1100$  MW,  $R = 0.015$  rad per sec/MW  
 Area B:  $P_D = 9,900$  MW,  $P_G = 10,000$  MW  $R = 0.0015$  rad per sec/MW  
 Load change: 20 MW decrease in Area A

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**Example**

- The generators in each area respond:

$$\Delta P_{GA} = -\frac{1}{R_A} \Delta\omega = -\frac{1}{0.015} (0.0273) = -1.818 \text{ MW}$$

$$\Delta P_{GB} = -\frac{1}{R_B} \Delta\omega = -\frac{1}{0.0015} (0.0273) = -18.18 \text{ MW}$$

Area A      Area B

- Tie-line change:

$$\Delta P_{AB} = -\Delta P_{AB} = \Delta P_{GA} - \Delta P_{LA} = -1.818 + 20 = 18.182 \text{ MW}$$

Area A:  $P_D = 1000$  MW,  $P_G = 1000$  MW,  $R = 0.015$  rad per sec/MW  
 Area B:  $P_D = 9,900$  MW,  $P_G = 10,000$  MW  $R = 0.0015$  rad per sec/MW  
 Freq. Change: 0.0273

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**Example**

- Now for the ACE

$$ACE_A = \Delta P_{AB} + \frac{1}{R_A} \Delta\omega = 18.182 + \left(\frac{1}{0.015}\right)(0.0273) = 18.182 + 1.82 = 20 \text{ MW}$$

$$ACE_B = \Delta P_{BA} + \frac{1}{R_B} \Delta\omega = -18.182 + \left(\frac{1}{0.0015}\right)(0.0272) = 0 \text{ MW}$$

Area A      Area B

Area A:  $P_D = 1000$  MW,  $P_G = 1000$  MW,  $R = 0.015$  rad per sec/MW  
 Area B:  $P_D = 9,900$  MW,  $P_G = 10,000$  MW  $R = 0.0015$  rad per sec/MW  
 Freq. Change: 0.0273  
 $\Delta P_{AB}$ : 18.182 MW

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**Frequency Control**

- Extension to n-area case:

$$ACE_i = \sum_{j=1}^n \Delta P_{ij} + B_i \Delta\omega$$

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