

15-System Model

Text: 5.8 – 5.11

ECEGR 451
Power Systems

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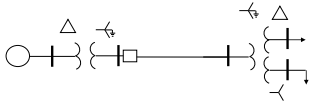
Topics

- One-line Diagram
- System Modeling
- Example
- Regulating Transformers

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One-Line Diagram

- Generator
- Bus
- Transformer
- Transmission line
- Circuit breaker
- Load

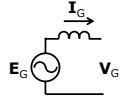


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One-Line Diagram

- Simple generator model:

V_G : terminal voltage
 E_G : open circuit voltage
 I_G : generator current



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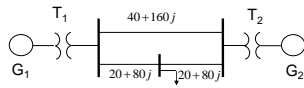
System Model

- We've discussed transmission lines, transformers, per unit, one line diagrams
- Now we put them all together to model the system

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System Model

- G_1 : 50 MVA, 12.2 kV, $X = 0.15$ p.u.
- G_2 : 20 MVA, 13.8 kV, $X = 0.15$ p.u.
- T_1 : 80 MVA 12.2/161 kV, $X = 0.10$ p.u.
- T_2 : 40 MVA 13.8/161 kV, $X = 0.10$ p.u.
- Load: 50 MVA, 0.80 PF (lagging), operating at 154 kV



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1. Pick a power base for the system

- Common to select power base equal to or near the largest generator in the system
- Let $S_B = 100$ MVA (three phase)

$T_1: 80 \text{ MVA } 12.2/161 \text{ kV}, X = 0.10 \text{ p.u.}$
 $T_2: 40 \text{ MVA } 13.8/161 \text{ kV}, X = 0.10 \text{ p.u.}$

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2a. Select voltage base

- Common to select voltage base equal to or near the line-line voltage at any section
 - Must keep track of voltage base and section
 - Sections are separated by transformers
- Let $V_B = 132$ kV (line-line) at the transmission line section

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2b. Compute voltage bases for all sections

- Use transformer ratios (line-line) to relate base voltages between sections
- G1 section: $V_{1B} = 132 \times (12.2/161) = 10.002$ kV
- G2 section: $V_{2B} = 132 \times (13.8/161) = 11.31$ kV

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3. Express all impedances in consistent p.u. terms

- All sections have same power bases, but different voltage bases
- Impedances are given with different power and voltage bases
- Convert using: $Z_{p.u.}^{new} = Z_{p.u.}^{old} \left(\frac{V_B^{old}}{V_B^{new}} \right)^2 \frac{S_B^{new}}{S_B^{old}}$

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3. Express all impedances in consistent p.u. terms

- $G_1: X = 0.15 \times (100/50) \times (12.2/10.002)^2 = 0.4463 \text{ p.u.}$
- $G_2: X = 0.15 \times (100/20) \times (13.8/11.31)^2 = 1.1166 \text{ p.u.}$
- $T_1: X = 0.1 \times (100/80) \times (12.2/10.002)^2 = 0.1 \times (100/80) \times (161/132)^2 = 0.18596 \text{ p.u.}$
- $T_2 = 0.1 \times (100/40) \times (13.8/11.31)^2 = 0.3719 \text{ p.u.}$

$$Z_{p.u.}^{new} = Z_{p.u.}^{old} \frac{S_B^{new}}{S_B^{old}} \left(\frac{V_B^{old}}{V_B^{new}} \right)^2$$

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3. Express all impedances in consistent p.u. terms

- The transmission line and load:
 - $Z_{3B} = (132)^2/100 = 174.24 \text{ p.u.}$
 - $Z_{line,a} = (40 + j160)/174.24 = 0.2296 + j0.9183$
 - $Z_{line,b} = (20 + j80)/174.24 = 0.1148 + j0.4591 \text{ p.u.}$
- and for the load:
 - $S = 50(.8 + j.6) = 40 + 30j \text{ MVA}$
 - $Z_{load} = \{(154)^2/(40 + 30j)\}^* = 379.456 + j284.529 = 2.18 + j1.63 \text{ p.u.}$

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4a. Draw the impedance diagram

- Redrawing the system

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4b. Solve for desired quantities

- Use per-phase analysis

impedance diagram

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5. Convert back to actual quantities, if needed

impedance diagram

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Example

- Specifications
 - G_1 : 75 MVA, 10 kV, $X = 0.10$ p.u.
 - G_2 : 75 MVA, 22 kV, $X = 0.08$ p.u.
 - T_1 : 75 MVA 10/365 kV, $X = 0.12$ p.u.
 - T_2 : 80 MVA 24/380 kV, $X = 0.14$ p.u.
 - Load: $I_{load} = 118.6 \angle -10^\circ$ A
 - $E_{G2} = 25 \angle 0^\circ$ kV
- Choose $V_B = 365$ kV at the transmission line and $S_B = 75$ MVA

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Example

- Section base voltages:
 - $V_{B3} = 365$ kV
 - $V_{B1} = 10$ kV
 - $V_{B2} = 23.05$ kV

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Example

- New generator impedances
 - $Z_{p.u.}^{new} = Z_{p.u.}^{old} \left(\frac{V_B^{old}}{V_B^{new}} \right)^2 \frac{S_B^{new}}{S_B^{old}}$
 - $X_{G1} = 0.1 \left(\frac{10}{10} \right)^2 \frac{75}{75} = 0.1$
 - $X_{G2} = 0.08 \left(\frac{22}{23.05} \right)^2 \frac{75}{75} = 0.073$

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Example

- New transformer impedances

$$\mathbf{z}_{p.u.}^{new} = \mathbf{z}_{p.u.}^{old} \left(\frac{V_B^{old}}{V_B^{new}} \right)^2 \frac{S_B^{new}}{S_B^{old}}$$

$$X_{T1} = 0.12 \left(\frac{10}{10} \right)^2 \frac{75}{75} = 0.12$$

$$X_{T2} = 0.14 \left(\frac{24}{23.05} \right)^2 \frac{80}{75} = 0.1423$$

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Example

- Transmission line impedance in p.u.

$$Z_B = \frac{V_B^2}{S_B} = \frac{365k^2}{75M} = 1776.3\Omega$$

$$\mathbf{z}_{L1} = \frac{26 + j178}{1776.3} = 0.015 + j0.1$$

$$\mathbf{z}_{L2} = \frac{j35}{1776.3} = j0.02$$

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Example

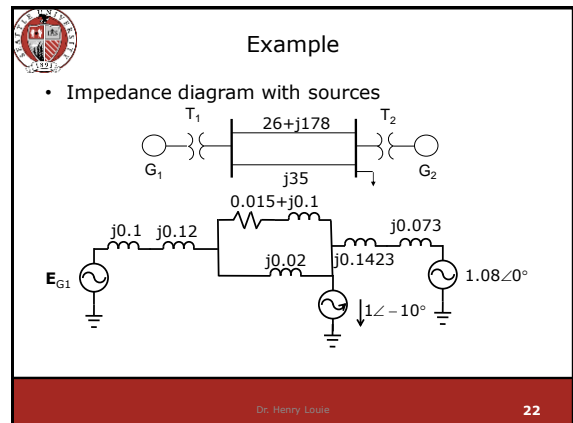
- Load current and generator 2 voltage

$$I_B = \frac{S_B}{\sqrt{3}V_B} = 118.6A$$

$$\mathbf{I}_{load} = \frac{118.6 \angle -10^\circ}{I_B} = 1 \angle -10^\circ$$

$$\mathbf{E}_{G2} = \frac{25 \angle 0^\circ}{23.05} = 1.08 \angle 0^\circ$$

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Regulating Transformers

- We can now describe the system model in per unit with the impedance diagram
- We have seen that using per unit on normal systems, we have eliminated the transformers
- However, this is not a general result as there are some transformers that do not "disappear" when per unit normalization is used
 - regulating and off-nominal transformers

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Regulating Transformers

- Transformers used to adjust voltage magnitude or phase are called "regulating transformers"
- They do this by adding a small amount (+ or - 10 %) of voltage to the line or phase voltages
- Voltage can also be changed by adjusting the turns ratio of the transformer (called tap changing)
- Tap changing may be automatic and may occur while the transformer is energized (load-tap-changing)

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Regulating Transformers

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Regulating Transformer

$$\mathbf{V}_{a'n} = \mathbf{V}_{an} + \Delta\mathbf{V}_{an}$$

$$\mathbf{V}_{b'n} = \mathbf{V}_{bn} + \Delta\mathbf{V}_{bn}$$

$$\mathbf{V}_{c'n} = \mathbf{V}_{cn} + \Delta\mathbf{V}_{cn}$$

voltage magnitude increase

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Phase-Shifting Transformer

- Basic idea: add a voltage that is 90 degrees out of phase

$$\mathbf{V}_{bc} = \sqrt{3}\mathbf{V}_{an}e^{-j\frac{\pi}{2}} \quad \mathbf{V}_{a'n} = \mathbf{V}_{an} \left(1 + p\sqrt{3}e^{-j\frac{\pi}{2}} \right) = \mathbf{V}_{an} (1 - jp\sqrt{3})$$

- Phase shift, and small voltage magnitude change occur

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Off-Nominal Turns Ratio

- Consider two transformers in parallel with different ratios
- Assume system is per unit normalized to T_1 ratio, n
 - T_1 disappears from the impedance circuit
 - assume T_2 has the ratio n' (off-nominal)
 - define: $\bar{n} = n'/n$
- $T_1: X = 0.2$
- $T_2: X = 0.4, n'$ is such that $\bar{n} = 1.05$
- Load: $\mathbf{V}_2 = 1 \angle 0^\circ$
- $\mathbf{I}_{load} = 1.05 \angle -45^\circ$

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Off-Nominal Turns Ratio

- T_2 does not disappear from the circuit, we must include it using a transformer model
- How does arrangement affect power flows through each transformer?

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Off-Nominal Turns Ratio

- Using KVL and KCL:

$$\mathbf{I}_1 + \mathbf{I}_2 = 1.05 \angle -45^\circ$$

$$\mathbf{V}_1 = 1 \angle 0^\circ + j0.2\mathbf{I}_1 = \frac{1}{1.05} \angle 0^\circ + j0.4(1.05\mathbf{I}_2)$$

$$= -j0.2\mathbf{I}_1 + j0.42\mathbf{I}_2 = 0.0476$$

$$\mathbf{I}_1 = 0.5030 - j0.4262$$

$$\mathbf{I}_2 = 0.2395 - j0.3163$$

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Off-Nominal Turns Ratio

- Finding the power:

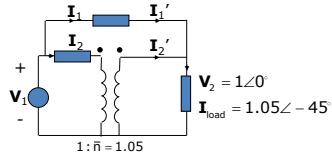
$$S_{i_1} = V_1 I_1' = 0.5030 + j0.4262$$

$$S_{i_2} = V_2 I_2' = 0.2395 + j0.3163$$

- If the turns ratios were the same:

$$S_{i_1} = 0.4950 + j0.4950 \quad \text{note the large}$$

$$S_{i_2} = 0.2475 + j0.2475 \quad \text{affect on VARS}$$



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Summary

- The system model procedure discussed takes a one line diagram of a power system and produces an impedance diagram
 - per unit is convenient and lends itself to three phase or single phase quantities
 - most transformers disappear from the system
- Regulating transformers can be used to adjust real and reactive power flows through the system
- Next lecture we begin to focus on two other representations of the system using network matrices

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