

## 13-Transformer Review

Text: 5.1 – 5.3

ECEGR 451  
Power Systems

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## Overview

- Transformers
- Ideal Single-Phase
- Non-Ideal Single Phase
- Three-Phase Transformers
- Normal Systems

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## Introduction



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## Introduction

- Transformers are important electrical-electrical energy conversion components
- One important reason we use AC is because we can easily change the voltage levels, which reduces losses
- Transformers enable this conversion of voltage level
  - High efficiency (up to 99%)
  - No or few moving parts (low maintenance)

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## Transformers

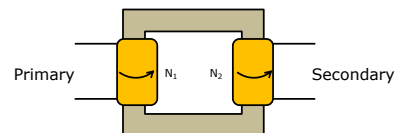
- Shift between voltage levels
  - generation 11 kV to 30 kV
  - transmission up to 765 kV
  - distribution around 69 kV
  - residential 240/120 V

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## Ideal Single-Phase Transformer

- Two magnetically coupled coils
  - Primary:  $N_1$  turns
  - Secondary:  $N_2$  turns
- Primary and secondary can be arbitrarily assigned
- Note direction of windings



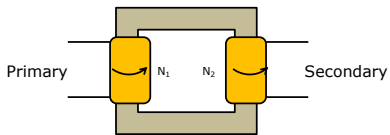
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### Ideal Single-Phase Transformer

**Ideal assumptions**

- No flux leakage
- No eddy currents
- No winding resistance
- Near infinite core permeability



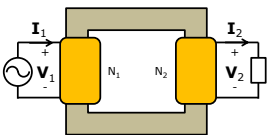
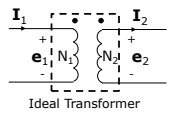
Primary N<sub>1</sub> N<sub>2</sub> Secondary

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### Single-Phase Transformer

- Recall

$$\frac{V_1}{V_2} = \frac{N_1}{N_2} \triangleq a \triangleq \frac{1}{n}$$

$$\frac{I_2}{I_1} = \frac{N_1}{N_2} = a$$



Ideal Transformer

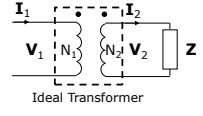
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### Circuit Model

- Now a load is connected to the secondary
- Solving for  $I_1$

$$I_1 = \frac{1}{a} I_2$$

$$I_1 = \frac{1}{a} \frac{V_2}{Z} \text{ using } I_2 = \frac{V_2}{Z}$$

$$I_1 = \frac{V_1}{a^2 Z} \text{ using } V_1 = a V_2$$


Ideal Transformer

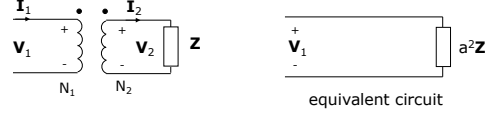
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### Circuit Model

From this result, it is possible to analyze the circuit only using primary-side voltage and current ( $V_1, I_1$ )

$$I_1 = \frac{V_1}{a^2 Z}$$

Secondary impedance referred to the primary side

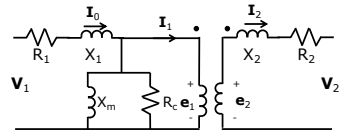


equivalent circuit

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### Non-Ideal Model

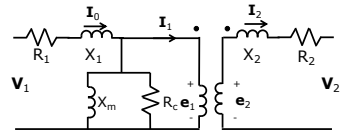
- Transformer non-idealities:
  - Winding resistance
  - Leakage reactance
  - Magnetizing reactance
  - Core loss



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### Non-Ideal Model

- For most transformers:
  - $R_c > X_m$
  - $R_1 < X_1, R_2 < X_2$



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### Three-Phase Transformer Connections

- We are generally more concerned with three phase transformers
- Three-phase transformers can be composed of three single-phase transformers or be wound on the same core
- Many combinations are possible:
  - Y-Y
  - Delta-Delta
  - Y-Delta
  - Delta-Y

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### Y-Y Transformer

- Each side has a common point, n or n'
- Neutral points usually grounded
- Line-Neutral voltages appear across the coils on each side

Do not confuse this n with 1/a → n

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### Y-Y Transformer Analysis

Phasor Diagram for Ideal Y-Y Connected Transformer

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### Three-Phase Transformer Analysis: Y-Y

- Let k be the transformer voltage gain
- For Y-Y transformers:
 
$$V_{a'n'} = kV_{an} = \frac{N_2}{N_1} V_{an}$$
 therefore  $k = n$  ← Do not confuse this n with the neutral point
 
$$I_a = \frac{I'_a}{k} = \frac{I'_a}{n}$$

$$V_{a'b'} = nV_{ab}$$

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### Three-Phase Transformer Analysis: Y-Y

- Phase voltages
 
$$V_{a'n'} = nV_{an}, V_{b'n'} = nV_{bn}$$

$$V_{b'n'} = nV_{bn}, V_{c'n'} = nV_{cn}$$

$$V_{c'n'} = nV_{cn}, V_{c'a'} = nV_{ca}$$
- Line currents
 
$$I_a = \frac{I'_a}{n}$$

$$I_b = \frac{I'_b}{n}$$

$$I_c = \frac{I'_c}{n}$$
 Recall: phase currents = line current for Y connections

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### Per-Phase Y-Y Analysis

- Three phase non-ideal Y-Y transformer model
- Want to model as per-phase equivalent

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### Per Phase Y-Y Analysis

- Per-phase equivalent of non-ideal Y-Y transformer
- Analyze like a single-phase transformer

ideal xfmr

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### Δ-Δ Transformer

- No neutral point
- $V_{ab}$ ,  $V_{a'b'}$  in phase
- $I_{abr}$ ,  $I_{a'b'}$  in phase
  - Similar results for b, c phase
- Line-line voltages appear across the coils on primary and secondary

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### Three-Phase Transformer Analysis: Δ-Δ

- Let  $k$  be the transformer voltage gain
- For Δ-Δ transformers:
 
$$V_{a'b'} = kV_{ab} = \frac{N_2}{N_1} V_{ab}$$
 therefore  $k = n$ 

$$I_{a'b'} = \frac{I_{ab}}{k} = \frac{I_{ab}}{n}$$

$$V_{a'n'} = nV_{an}$$

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### Three-Phase Transformer Analysis: Δ-Δ

- Voltage Relationships
 
$$V_{a'b'} = nV_{ab}$$

$$V_{b'c'} = nV_{bc}$$

$$V_{c'a'} = nV_{ca}$$
- Current Relationships
 
$$I_a = \frac{I_a}{n}, I_{b'a'} = \frac{I_{ab}}{n}$$

$$I_b = \frac{I_b}{n}, I_{c'b'} = \frac{I_{bc}}{n}$$

$$I_c = \frac{I_c}{n}, I_{a'c'} = \frac{I_{ca}}{n}$$

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### Per-Phase Δ-Δ Transformer

- Need to convert each side of the transformer to Y
- Recall that:  $z_y = \frac{z_\Delta}{3}$
- Per-phase equivalent circuit of non-ideal Δ-Δ transformer

ideal xfmr

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### Δ-Y Transformer

- Secondary has a neutral connection
- Line-line voltages appear on the coils on primary
- Line-neutral voltages appear on the coils on the secondary
- Less insulation needed on HV winding

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### Δ-Y Transformer Analysis

Phasor Diagram for Ideal Delta-Y Connected Transformer

30° phase shift from primary to secondary

Magnitudes shown assuming  $N_1 < N_2$

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### Delta-Y Transformer Analysis

Phasor Diagram for Ideal Delta-Y Connected Transformer

$I_a = I_{ab} - I_{ca}$   
 $I_b = I_{bc} - I_{ab}$   
 $I_c = I_{ca} - I_{bc}$

30° phase shift from primary to secondary

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### Three-Phase Transformer Analysis: Delta-Y

- Let  $k$  be the transformer voltage gain
- For  $\Delta$ -Y transformers:
 
$$V_{a'n'} = nV_{ab} = nV_{an}\sqrt{3}e^{j\frac{\pi}{6}} = kV_{an}$$
 therefore  $k = n\sqrt{3}e^{j\frac{\pi}{6}}$  Important result!

$$I_{a'} = \frac{I_{ab}}{n} = \frac{I_a e^{j\frac{\pi}{6}}}{\sqrt{3}n}$$

$$= \frac{I_a}{k'}$$

} same phase shift as voltage

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### Delta-Y Transformer Analysis

- Voltage relationships
 
$$V_{a'n'} = kV_{an}, \quad V_{a'b'} = kV_{ab}$$

$$V_{b'n'} = kV_{bn}, \quad V_{b'c'} = kV_{bc}$$

$$V_{c'n'} = kV_{cn}, \quad V_{c'a'} = kV_{ca}$$
- Line current relationships
 
$$I_{a'} = \frac{I_a}{k'}$$

$$I_{b'} = \frac{I_b}{k'}$$

$$I_{c'} = \frac{I_c}{k'}$$

primary                  secondary

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### Y-Δ Transformer

- No neutral point on secondary
- Line-Neutral voltage across primary coils
- Line-Line voltage across secondary coils

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### Three-Phase Transformer Analysis: Y-Δ

- Let  $k$  be the transformer voltage gain
- For Y- $\Delta$  transformers:
 
$$V_{a'b'} = nV_{an} = \frac{nV_{ab}e^{-j\frac{\pi}{6}}}{\sqrt{3}} = kV_{ab}$$
 therefore  $k = \frac{ne^{-j\frac{\pi}{6}}}{\sqrt{3}}$  Important result

Note: phase shift is  $-30^\circ$ , whereas for Delta-Y transformer connection in previous slides it is  $+30^\circ$

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### Three-Phase Transformer Analysis

- It can be shown for line currents:

$$\left. \begin{aligned} \mathbf{I}_{a'} &= \frac{\mathbf{I}_a}{k'} \\ \mathbf{I}_{b'} &= \frac{\mathbf{I}_b}{k'} \\ \mathbf{I}_{c'} &= \frac{\mathbf{I}_c}{k'} \end{aligned} \right\} \text{same phase-shift as voltages}$$

primary          secondary

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### Question

Is there any concern in connecting a three phase Y-Delta transformer in parallel with a three phase Delta-Y transformer? Assume the transformers are appropriately rated.

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### Three-Phase Transformer Analysis

- What about power?

$$\mathbf{S} = \mathbf{V}_{an'} \cdot \mathbf{I}_a = k \mathbf{V}_{an} \left( \frac{\mathbf{I}_a}{k'} \right) = \mathbf{V}_{an} \mathbf{I}_a' \text{ for all configurations}$$

- For ideal three-phase xfmr's, power is conserved, as in the single phase case

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### Three-Phase Transformer Analysis

- What about impedances?
- For all transformer connections:

$$\text{secondary impedance referred to the primary} = \frac{1}{|k|^2} \mathbf{Z}_l$$

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### Transformer Phase Shifts

- Various winding connections of  $\Delta$ -Y, and Y- $\Delta$  xfmr's lead to different phase shifts
- Standard is to have **phase-neutral voltages advance** by 30 degrees when going from low voltage to high voltage
- Previous slides have followed this convention

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### Per-Phase Analysis ( $\Delta$ -Y)

- Per-phase equivalent of a non-ideal  $\Delta$ -Y transformer
- Complex ideal transformer with gain  $k$  or  $k^*$

$$k = \sqrt{3} n e^{j\frac{\pi}{6}}$$

- +30° shift when primary is lower voltage and secondary is higher voltage

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### Per-Phase Analysis (Y-Δ)

- Per-phase equivalent of a Y-Δ transformer
- Complex ideal transformer with gain  $k$  or  $k^*$ 

$$k = \frac{ne^{j\pi/6}}{\sqrt{3}}$$
  - +30° shift when primary is lower voltage and secondary is higher voltage

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### Normal Systems

- Parallel paths in the transmission network can result in circulating currents
- At the heart of the problem are the phase shifts and voltage ratios in transformers
- Systems that are "normal" avoid these problems
- A system is normal if, for each parallel path
  - the product of ideal transformer gain magnitudes is the same
  - the sum of ideal transformer phase shifts is the same

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### Normal Systems

- $V_1$ : line-neutral = 8000 V
- Y-Y:  $n = 10, X_L = 0.05$
- Y-Δ:  $n = 10\sqrt{3}, X_L = 0.05$
- Find  $|I_1|, |I_2|, |I_{load}|$

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### Normal Systems

- KVL for  $I_1$  loop:
 
$$V_1 = j0.05I_1 + V_x$$

$$= j0.05I_1 + \frac{1}{10}100 I_1' + I_2'$$

$$V_1 = 10 + j0.5 I_1 + 10I_2 = 8000\angle 0^\circ \text{ V}$$
 replacing  $I_1$  with  $10I_1'$

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### Normal Systems

- KVL around  $I_2$  loop:
 
$$V_1 = j0.05I_2 + \frac{1}{10}e^{-j\pi/6} 100 I_1' + I_2'$$

$$V_1 = 10I_1'e^{j\pi/6} + 10 + j0.5 I_2'e^{-j\pi/6}$$
 replacing  $I_2$  with  $10I_2'e^{-j\pi/6}$ 

$$10I_1' + 10 + j0.5 I_2' = 8000\angle 30^\circ$$
 shifting by 30 deg.

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### Normal Systems

- Solving:
 
$$10I_1' + 10 + j0.5 I_2' = 8000\angle 30^\circ$$

$$10 + j0.5 I_1' + 10I_2' = 8000$$
- Yields
  - $I_1' = 3755.0\angle -164.85^\circ \text{ A}$
  - $I_2' = 4527.2\angle 14.88^\circ \text{ A}$
  - $I_{load} = 772.5\angle 13.57^\circ \text{ A}$
- circulating current: only a small portion of the current flows into the load!

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### Normal Systems

