

07-Transmission Line Inductance

Text: 3.0 – 3.3

ECEGR 451
Power Systems

Dr. Henry Louie

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Topics

- Inductance
- Single-phase
- N-phase
- Symmetrical spacing

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Introduction

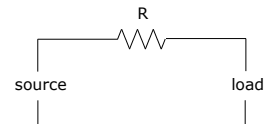
- Transmission lines form conductive loops
- Need to model inductance of transmission lines
 - Remember Maxwell's Equations?
- Tedious derivations follow

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Transmission Line

- Our transmission line model so far is limited
- Inductance and capacitance need to be modeled
- Start with inductance



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Inductance

- Derive expressions for inductance
 - internal
 - external
 - Geometry-specific
- Incorporate inductance into our line model

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Inductance

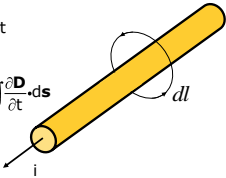


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Ampere's Law

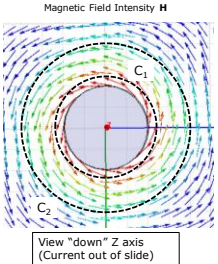
- Current through a conductor will produce a circular magnetic field around it
 - Line integral of the magnetic field around the conductor equals the current through it
- Mathematically

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} \quad \text{or} \quad \oint_C \mathbf{H} \cdot d\ell = \int_S \mathbf{J} \cdot d\mathbf{s} + \int_S \frac{\partial \mathbf{D}}{\partial t} \cdot d\mathbf{s}$$


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Ampere's Law

- Direction of \mathbf{H} field is CCW
 - Right Hand Rule
- Field strength decreases as path length increases
 - Field becomes weaker as distance increases

$$\oint_C \mathbf{H} \cdot d\ell = \oint_C \mathbf{H} \cdot d\ell = \text{constant}$$


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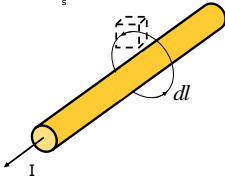
Magnetic Flux Density

- Related to \mathbf{H} is the Magnetic Flux Density (\mathbf{B})
- In linear isotropic homogeneous (LIH) medium
 - $\mathbf{B} = \mu_0 \mathbf{H}$
- where:
 - \mathbf{B} : magnetic flux density (Wb/m²)
 - μ_0 : permeability of free space $4\pi \times 10^{-7}$ (H/m)
 - μ_r : relative permeability

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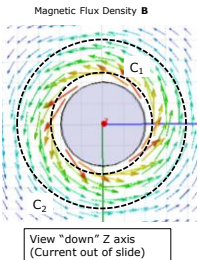
Gauss's Law for Magnetic Fields

- The magnetic flux entering a volume is equal to the magnetic flux leaving it (it is continuous)
- Mathematically
 - $\nabla \cdot \mathbf{B} = 0$ or $\oint_S \mathbf{B} \cdot d\mathbf{s} = 0$ (divergence is 0)



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Magnetic Flux Density

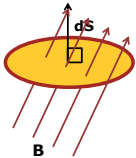


- Direction of \mathbf{B} field is in line with \mathbf{H} field
- Field strength decreases as path length increases
 - Field becomes weaker as distance increases

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Magnetic Flux

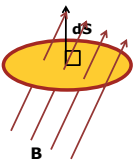
- The total magnetic flux, Φ , passing through a surface is:
 - $\Phi = \int_S \mathbf{B} \cdot d\mathbf{s}$
- where:
 - Φ : magnetic flux (Wb)



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Flux Linkages

The total flux linking a coil of wire with N turns is
 $\lambda = N\Phi$
 where:
 λ : flux linkage (Wb-Turns)
 N: number of turns (Turns)



B

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Inductance

Inductance is related to flux linkages as:

$$L \triangleq N \frac{d\phi}{di}$$

$$\lambda = N\Phi$$

$$\frac{d\lambda}{di} = \frac{Nd\phi}{di} \text{ (derivative wrt } i)$$

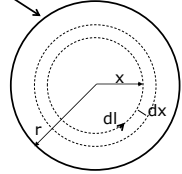
$$L = \frac{d\lambda}{di} \text{ (via substitution)}$$

We will derive an equation first for internal inductance.
 Note: subsequent derivation results in H/m, not H

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Internal Inductance

- Assume:
 - uniform current density
 - infinitely long
 - carries total current i (out of slide)
 - i_x current inside radius x



Key Equations

- $\oint H \times dl = i$
- $B = \mu H$
- $\phi = \int B \cdot da$

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Internal Inductance

$B_x = \frac{\mu x i}{2\pi r^2}$ flux density x at meters

$d\phi = \frac{\mu x i}{2\pi r^2} dx$ from eqn 3

$d\lambda = \frac{\pi x^2}{\pi r^2} d\phi$ only a fraction of the current is linked (not all of the current is affected by the linked flux)

$$= \frac{\mu i x^3}{2\pi r^4} dx \text{ via substitution}$$

$$\lambda_{int} = \int_0^r \frac{\mu i x^3}{2\pi r^4} dx$$

$$= \frac{\mu i}{8\pi}$$

Key Equations

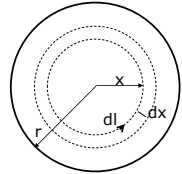
- $\oint H \times dl = i$
- $B = \mu H$
- $\phi = \int B \cdot da$

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Internal Inductance

$$\lambda_{int} = \frac{\mu i}{8\pi}$$

$$\lambda_{int} = \frac{1}{2} \times 10^{-7} \text{ Wbt/m evaluating constants}$$

$$L_{int} = \frac{1}{2} \times 10^{-7} \text{ H/m}$$


Key Equations

- $\oint H \times dl = i$
- $B = \mu H$
- $\phi = \int B \cdot da$

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External Inductance

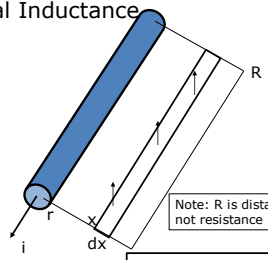
$H2\pi x = i$ from eqn. 1

$B = \frac{\mu i}{2\pi x}$ from eqn. 2

$\lambda_{ext} = \int_r^R B_x \times dx$ between r and R

$$= \mu_0 \int_r^R \frac{i}{2\pi x} dx \text{ via substitution}$$

Evaluate the integral



Key Equations

- $\oint H \times dl = i$
- $B = \mu H$
- $\phi = \int B \cdot da$

Note: R is distance, not resistance

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External Inductance

$H2\pi x = i$ from eqn. 1
 $B = \frac{\mu_0 i}{2\pi x}$ from eqn. 2
 $\lambda_{ext} = \int_r^R B_x \times dx$ between r and R
 $= \mu_0 \int_r^R \frac{i}{2\pi x} dx$ via substitution
 $= \frac{\mu_0 i}{2\pi} \ln \frac{R}{r}$

Note: R is distance, not resistance

Key Equations
 1. $\oint H \cdot dl = i$ 3. $\phi = \int B \cdot da$
 2. $B = \mu H$

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Inductance of a Infinite Wire

- Superposition of internal and external flux, inductance

$$\lambda = 2 \times 10^{-7} i \left(\frac{\mu_0}{4} + \ln \frac{R}{r} \right) \text{ Wb-turm/m}$$

$\frac{\mu_0}{4}$
internal
external

- Inductance is therefore:

$$L = 2 \times 10^{-7} \left(\frac{\mu_0}{4} + \ln \frac{R}{r} \right) \text{ H/m}$$

Note: derived flux linkages and inductance are per m

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Single-Phase Inductance

- Next we consider single-phase circuit inductance
- Single phase: "hot" conductor and "return" conductor

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Single-Phase Inductance

- Flux set up by conductor 1 at a distance greater than $D+r_2$ does not link the circuit
- Approximation: use D instead of $(D-r_1)$ or $(D-r_2)$
- L_1 : inductance due to conductor 1 only

$$L = 2 \times 10^{-7} \left(\frac{\mu_0}{4} + \ln \frac{R}{r} \right)$$

$$L_1 = \left(\frac{1}{2} + 2 \ln \frac{D}{r_1} \right) \times 10^{-7} \text{ H/m} \quad \text{assuming } \mu_r = 1$$

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Single-Phase Inductance

$$L_1 = \left(\frac{1}{2} + 2 \ln \frac{D}{r_1} \right) \times 10^{-7} \text{ H/m} \quad \text{let's clean this up a bit}$$

$$L_1 = 2 \left(\ln e^{\frac{1}{4}} + \ln \frac{D}{r_1} \right) \times 10^{-7} \text{ H/m} \quad \text{using } \ln e^{\frac{1}{4}} = \frac{1}{4}$$

$$L_1 = 2 \left(\ln \frac{D}{r_1 e^{-\frac{1}{4}}} \right) \times 10^{-7} \text{ H/m}$$

$$L_1 = 2 \left(\ln \frac{D}{r_1'} \right) \times 10^{-7} \text{ H/m} \quad \text{via substitution}$$

$r_1' = r_1 e^{-\frac{1}{4}} = 0.778 r_1$

Interpretation: r_1' is the radius of a fictitious conductor assumed to have no internal flux, but with the same inductance of the actual conductor of radius r_1

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Single-Phase Inductance


- What about the other conductor?
- Which direction is the flux going?
- Same direction: inductances can be added
- L is the loop inductance per m
- $\frac{1}{2} L$ is the inductance per conductor

$$L_2 = 2 \left(\ln \frac{D}{r_2} \right) \times 10^{-7} \text{ H/m}$$

$r_1' = r_1' = r_2'$ (standard assumption)

$$L = L_1 + L_2 = 4 \left(\ln \frac{D}{r_1'} \right) \times 10^{-7} \text{ H/m}$$


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Example

Compute the inductance for a single-phase line that is 1km long, with a conductor radius of 0.02 m. The conductors are 3 m apart.

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Example


Compute the inductance for a single-phase line that is 1km long, with a conductor radius of 0.02 m. The conductors are 3 m apart.

$r' = 0.02e^{-0.25} = 0.0156 \text{ m}$

$L = 1000 \times 4 \left(\ln \frac{D}{r'} \right) \times 10^{-7} = 1000 \times 4 \left(\ln \frac{3}{0.0156} \right) \times 10^{-7} \text{H} = 0.0021 \text{ H}$

What is the inductive reactance?

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Example

Compute the inductance for a single-phase line that is 1km long, with a conductor radius of 0.02 m. The conductors are 3 m apart.


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What is the inductive reactance?

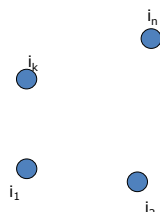
$X_L = 2\pi \times 60 \times 0.0021 = 0.79 \Omega$

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Many-Conductor Case

- Extend to multiple conductors: 1, ..., k, ..., n
- Assume distances between conductors is much greater than their radii
- Look at flux linkages of conductor 1 up to a radius R_1
- Add contributions of all other conductors



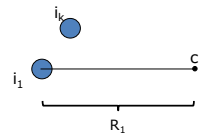
Note: n is a number, not the neutral

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General Case

- Start by examining the flux linking conductor 1 up to radius R_1
- First consider the k^{th} conductor

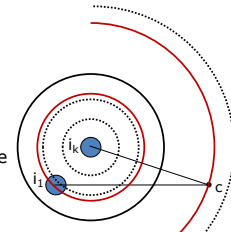


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General Case

- Flux from current in k^{th} conductor form concentric circles around it
- Only some flux from i^k has a net contribution to the total flux between conductor 1 and c (distance R_1)
 - Solid lines: contribute to net flux
 - Dashed lines: no net flux contribution



Flux between red lines have net contribution

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General Case

- Use point a to simplify the calculation
 - As R_1 increases, error decreases
- Therefore we consider the flux from conductor k between a and c

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General Case

- Need distance from center of conductor k to point a, and to point c

$$\lambda_{1k} = 2 \ln \left(\frac{R_k}{d_{1k}} \right) i_k \times 10^{-7}$$
- Next include other conductors

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General Case

- Including all conductors

$$\lambda_1 = 2 \left\{ i_1 \left(\frac{1}{4} + \ln \frac{R_1}{r_1} \right) + i_2 \ln \frac{R_2}{d_{12}} + \dots + i_n \ln \frac{R_n}{d_{1n}} \right\} \times 10^{-7}$$
 - conductor 1 (internal + external)
 - R_x : distance from conductor x to point c
 - d_{1x} : distance from conductor 1 to conductor x

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General Case

- What happens as $R_1 \rightarrow \infty$?
 - Assume: $i_1 + i_2 + \dots + i_k + \dots + i_n = 0$ (is this reasonable?)
 - Expanding:

$$\lambda_1 = 2 \left\{ i_1 \left(\frac{1}{4} + \ln \frac{R_1}{r_1} \right) + i_2 \ln \frac{R_2}{d_{12}} + \dots + i_n \ln \frac{R_n}{d_{1n}} \right\} \times 10^{-7}$$

$$\lambda_1 = 2 \left\{ i_1 \left(\frac{1}{4} + \ln \frac{1}{r_1} \right) + i_2 \ln \frac{1}{d_{12}} + \dots + i_n \ln \frac{1}{d_{1n}} \right\} \times 10^{-7} + 2 i_1 \ln R_1 + i_2 \ln R_2 + \dots + i_n \ln R_n \times 10^{-7}$$
 using $\ln \frac{x}{y} = \ln \frac{1}{y} + \ln x$

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General Case

- From previous slide:

$$\lambda_1 = 2 \left\{ i_1 \left(\frac{1}{4} + \ln \frac{1}{r_1} \right) + i_2 \ln \frac{1}{d_{12}} + \dots + i_n \ln \frac{1}{d_{1n}} \right\} \times 10^{-7} + 2 i_1 \ln R_1 + i_2 \ln R_2 + \dots + i_n \ln R_n \times 10^{-7}$$
- Note that:

$$0 = i_1 + i_2 + \dots + i_n$$

$$= -2 \ln(R_1) (i_1 + i_2 + \dots + i_n) \times 10^{-7}$$

$$= -2 i_1 \ln R_1 + i_2 \ln R_1 + \dots + i_n \ln R_1 \times 10^{-7} \text{ add this to } \lambda_1$$
- Yields

$$\lambda_1 = 2 \left\{ i_1 \left(\frac{1}{4} + \ln \frac{1}{r_1} \right) + i_2 \ln \frac{1}{d_{12}} + \dots + i_n \ln \frac{1}{d_{1n}} \right\} \times 10^{-7} + 2 \left\{ i_1 \ln \frac{R_2}{R_1} + i_2 \ln \frac{R_2}{R_1} + \dots + i_n \ln \frac{R_n}{R_1} \right\} \times 10^{-7}$$


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General Case

- As $R_1 \rightarrow \infty$, R_1 and R_x increase and become nearly equal and $\ln \left(\frac{R_k}{R_1} \right)$ becomes $\ln 1 = 0$
- Resulting in:

$$\lambda_1 = 2 \left\{ i_1 \left(\frac{1}{4} + \ln \frac{1}{r_1} \right) + i_2 \ln \frac{1}{d_{12}} + \dots + i_n \ln \frac{1}{d_{1n}} \right\} \times 10^{-7}$$

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General Case


- From last slide

$$\lambda_1 = 2 \left\{ i_1 \ln \frac{1}{4} + \ln \frac{1}{r_1} \right\} + i_2 \ln \frac{1}{d_{12}} + \dots + i_n \ln \frac{1}{d_{1n}} \times 10^{-7}$$
- via substitution

$$\lambda_1 = 2 \left\{ i_1 \ln \frac{1}{r_1'} + i_2 \ln \frac{1}{d_{12}} + \dots + i_n \ln \frac{1}{d_{1n}} \right\} \times 10^{-7}$$
- General kth conductor

$$\lambda_k = 2 \left\{ i_1 \ln \frac{1}{d_{k1}} + i_2 \ln \frac{1}{d_{k2}} + \dots + i_k \ln \frac{1}{r_k'} + \dots + i_n \ln \frac{1}{d_{kn}} \right\} \times 10^{-7}$$

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Equilateral Spacing

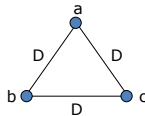
Assume
 $i_a + i_b + i_c = 0$
 find inductance per meter

use $\lambda_1 = 2 \left\{ i_1 \ln \frac{1}{r_1'} + i_2 \ln \frac{1}{d_{12}} + \dots + i_n \ln \frac{1}{d_{1n}} \right\} \times 10^{-7}$


$\lambda_a = 2 \left\{ i_a \ln \frac{1}{r_1'} + i_b \ln \frac{1}{D} + i_c \ln \frac{1}{D} \right\} \times 10^{-7}$

$\lambda_a = 2 \left\{ i_a \ln \frac{D}{r_1'} \right\} \times 10^{-7}$ Wbt/m using: $i_b \ln \frac{1}{D} + i_c \ln \frac{1}{D} = -i_a \ln D$

$L_a = 2 \left\{ \ln \frac{D}{r_1'} \right\} \times 10^{-7}$ H/m inductance per phase

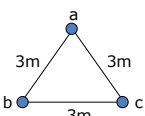


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Example

Compute the a-phase inductance of the line shown below if each conductor has a radius of 0.02m. Assume the line is 1km in length.

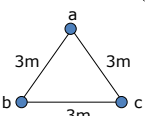


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Example

Compute the a-phase inductance of the line shown below if each conductor has a radius of 0.02m. Assume the line is 1km in length.

$$L_a = 1000 \times 2 \left\{ \ln \frac{D}{r_1'} \right\} \times 10^{-7} = 1000 \times 2 \left\{ \ln \frac{3}{0.0156} \right\} \times 10^{-7} = 0.00105H$$



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Observations

- For equilateral spacing and balanced conditions, only self inductances need to be modeled (no mutual inductance)
- Decreasing inductance can be accomplished by decreasing separation between phases or increasing the conductor radii

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Line Inductance Summary

- Developed expressions for internal and external inductance
- For single-phase lines

$$L = 2 \times 10^{-7} \left(\frac{\mu_r}{4} + \ln \frac{R}{r} \right)$$
- For equilateral (symmetrical) spacing

$$L = 4 \left(\ln \frac{D}{r_1'} \right) \times 10^{-7} \text{ H/m}$$

$$L_a = 2 \left\{ \ln \frac{D}{r_1'} \right\} \times 10^{-7} \text{ H/m}$$

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